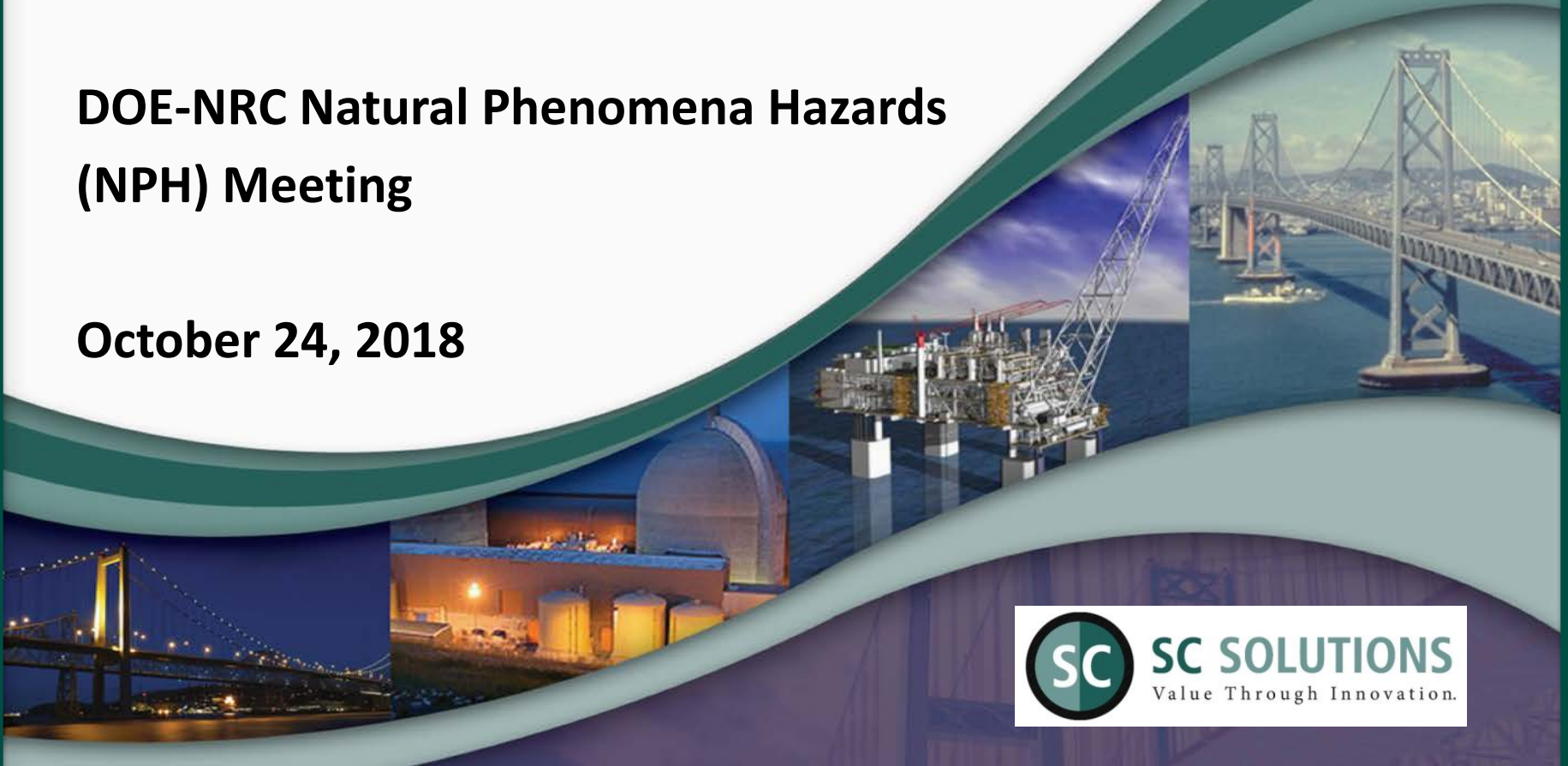


# Free Field Displacements Calculated with Green's Functions Implemented in SC-SASSI

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DOE-NRC Natural Phenomena Hazards  
(NPH) Meeting

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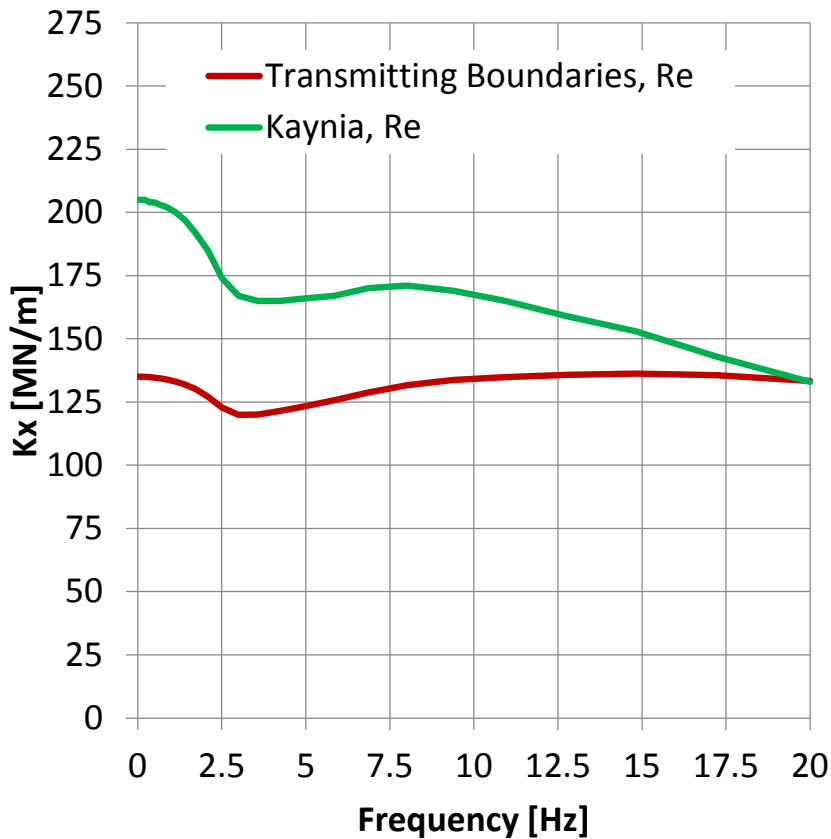


# Motivation: Can we simulate piles with SASSI?

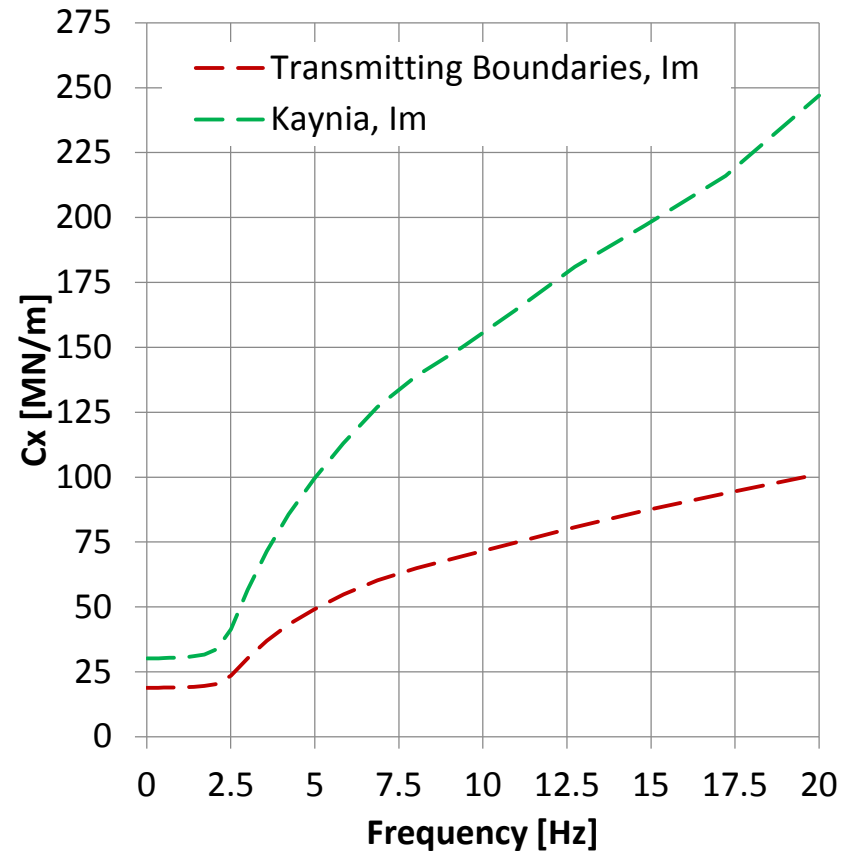
- SASSI: SSI analysis of shallow foundations
- Classic solutions for Piles (Thin Layer Method): Kaynia (1982), Hartmann (1985)
- Modeling shallow foundations vs pile foundations
- Calculation of soil displacements (flexibility) for one single node at each layer interface
- Semi-Analytical Displacement Formulation for:
  - Point Loads: Singularity (not defined) under the Load
  - Ring and Disk Loads: Defined under the load
- Green's Functions for distributed (Ring and Disk) loads approach represents better the load transfer from pile to soil than the Transmitting Boundaries (Point Load) approach.
- Focus of the presentation

# Dynamic Stiffness of Single Pile with Transmitting Boundaries

## Real Component



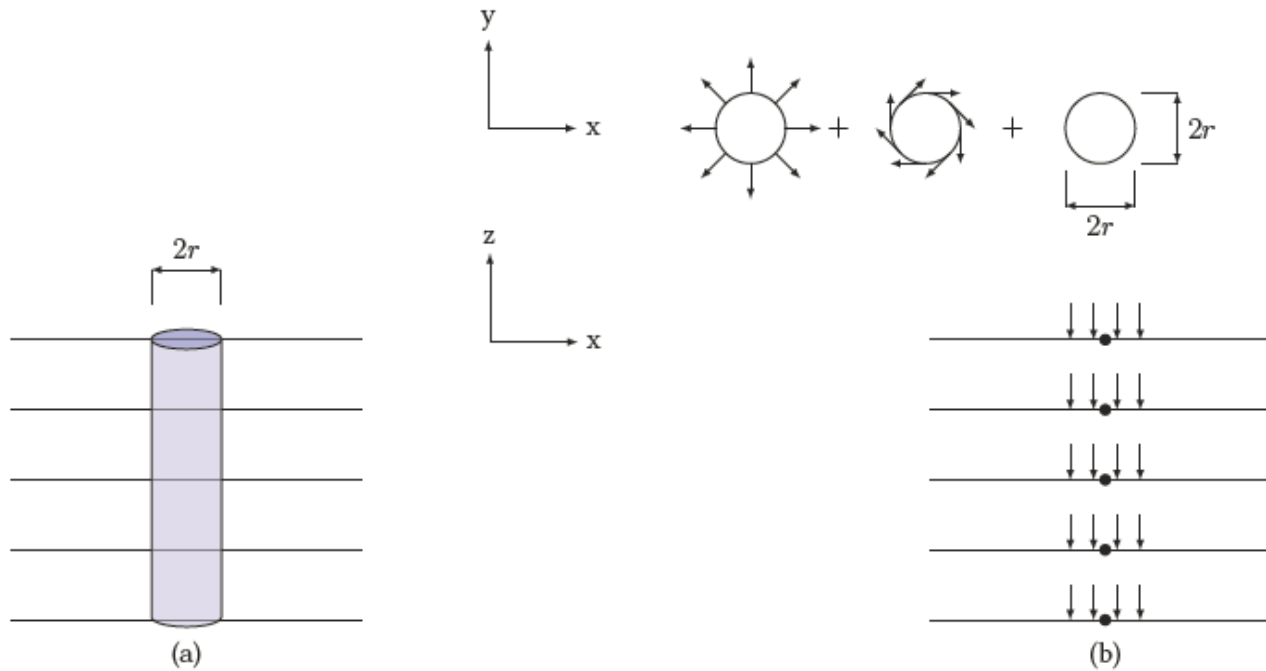
## Imaginary Component



**Transmitting Boundary (TB) approach underestimates the Dynamic Stiffness of Piles**

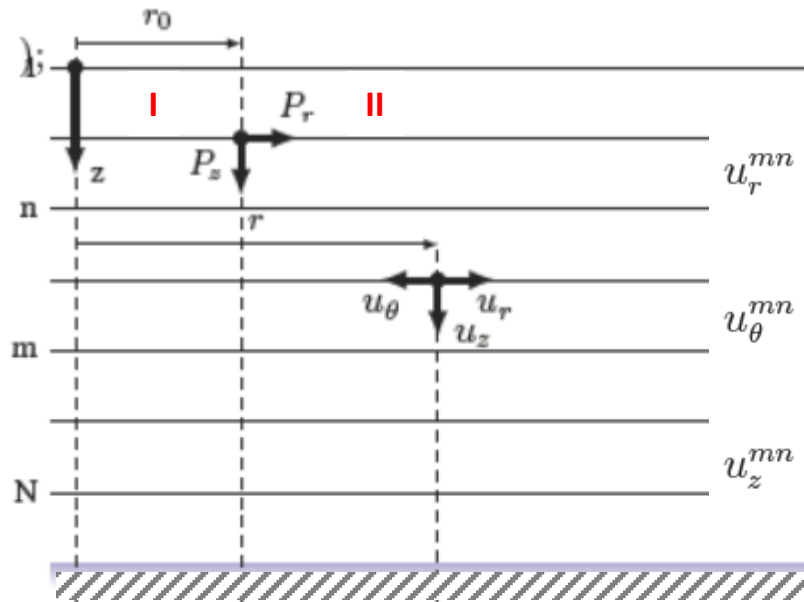
# Motivation: Pile Simulations

- Goals: Realistic estimation of soil flexibility for piles
- Efficient computational approach to simulate piles



# Theoretical Background

# Displacements due to Ring/Disk Loads

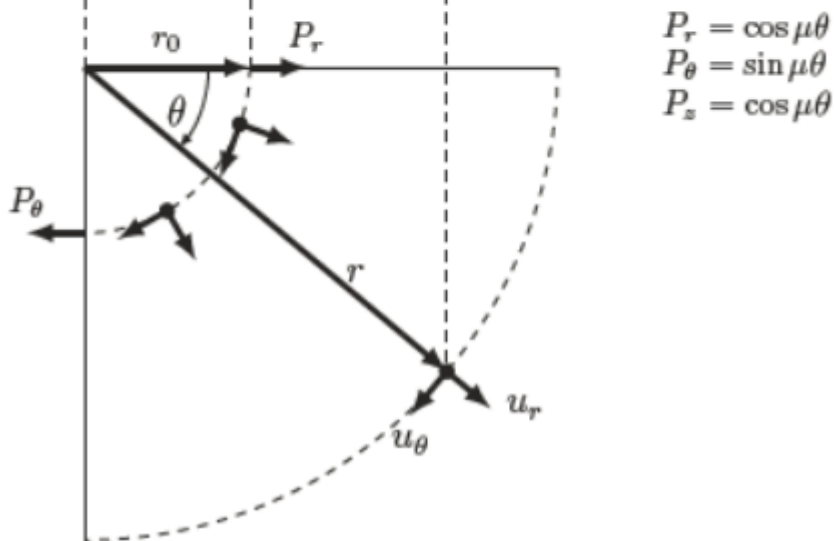


## Green's Functions

$$u_r^{mn} = \left\{ \sum_{l=1}^{2N} \alpha_R^{nl} \phi_x^{ml} \frac{d}{dr} f_l^R + \frac{\mu}{r} \sum_{l=1}^N \alpha_L^{nl} \phi_y^{ml} f_l^L \right\} \begin{bmatrix} \cos \mu\theta \\ \sin \mu\theta \end{bmatrix}$$

$$u_\theta^{mn} = \left\{ \frac{\mu}{r} \sum_{l=1}^{2N} \alpha_R^{nl} \phi_x^{ml} f_l^R + \sum_{l=1}^N \alpha_L^{nl} \phi_y^{ml} \frac{d}{dr} f_l^L \right\} \begin{bmatrix} -\sin \mu\theta \\ \cos \mu\theta \end{bmatrix}$$

$$u_z^{mn} = \left\{ -\sum_{l=1}^{2N} \alpha_R^{nl} \phi_z^{ml} f_l^R k_l \right\} \begin{bmatrix} \cos \mu\theta \\ \sin \mu\theta \end{bmatrix}$$



$$\begin{aligned} P_r &= \cos \mu\theta \\ P_\theta &= \sin \mu\theta \\ P_s &= \cos \mu\theta \end{aligned}$$

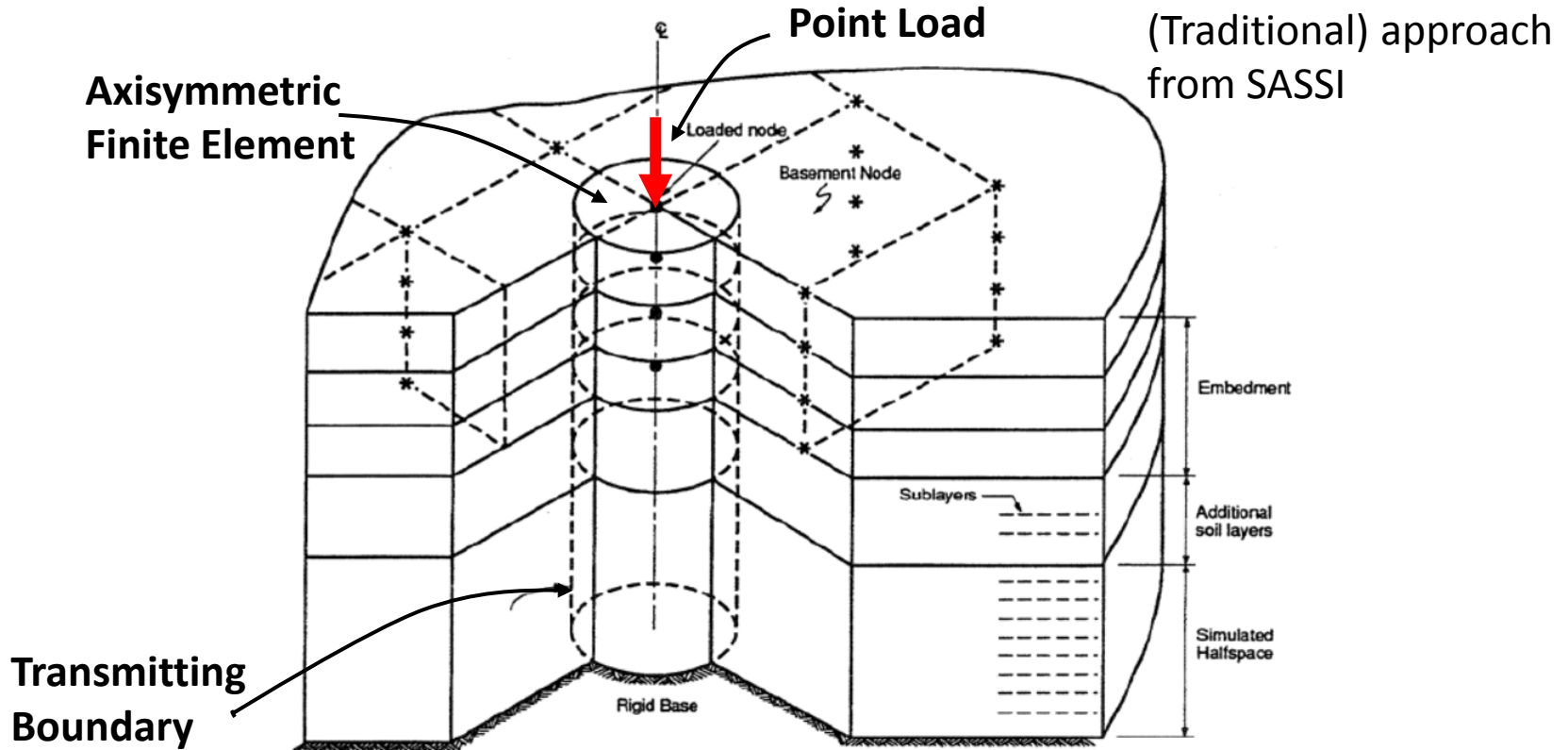
After Kausel (1981) and Waas (1980).

## Impedance Analysis

$$\left[ \tilde{\mathbf{K}}_{ii}^d \right] = \left[ \tilde{\mathbf{F}}_{ii}^d \right]^{-1}$$

Recently implemented in SC-SASSI

# Transmitting Boundaries (TB) and Finite Element



EXPLANATION  
\* Interaction Node

After Lysmer et. al (1981)

$$\left[ \tilde{\mathbf{K}}_{ii}^d \right] = \left[ \tilde{\mathbf{F}}_{ii}^d \right]^{-1}$$

# **Example: Soil Displacements**

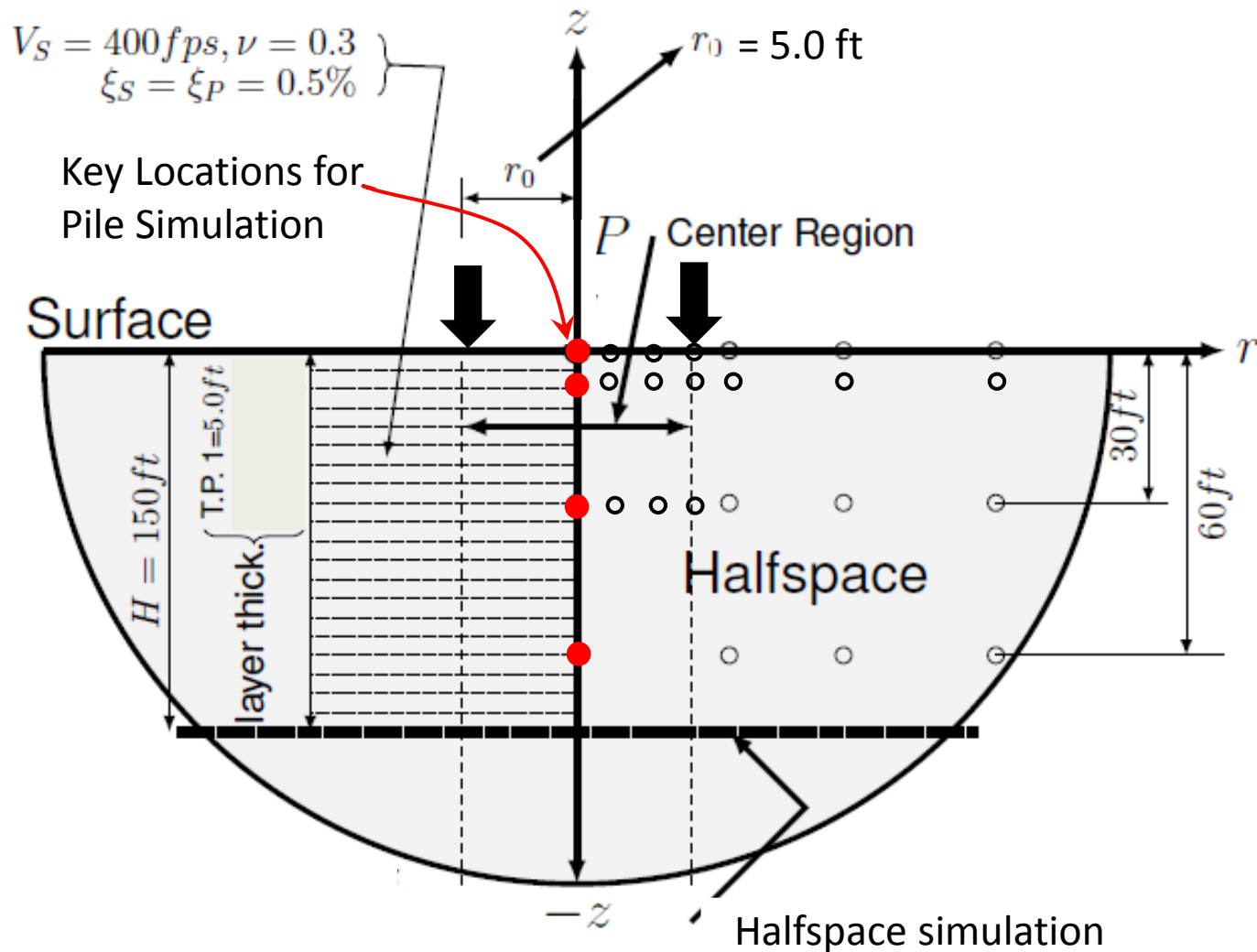
## **Objectives:**

**Limitations of Transmitting Boundaries inside the area of the load**

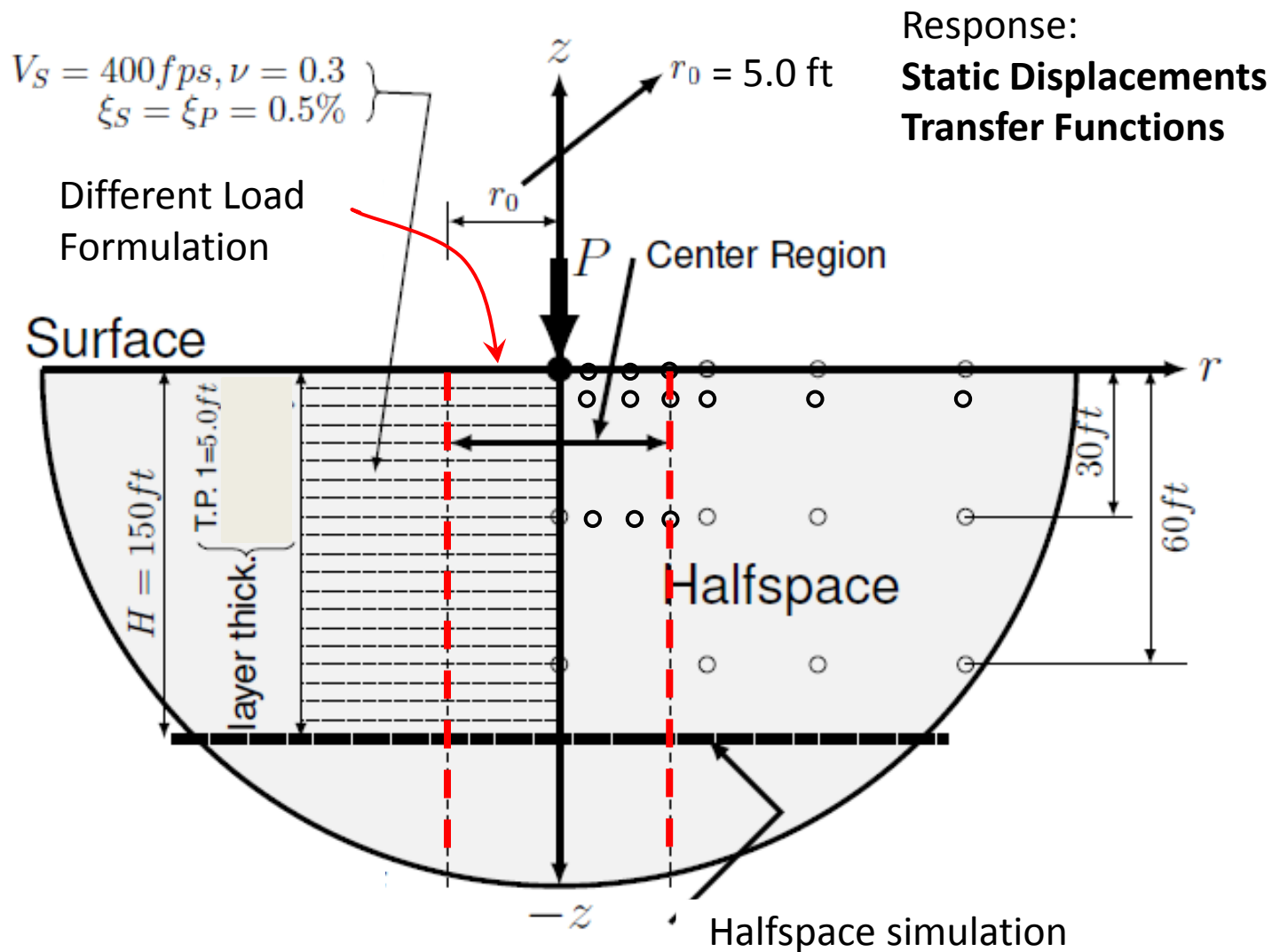
**Ring Load behaves like Point Load at distance and depth from load location**



# Example: Displacements (GF) due to Ring Loads



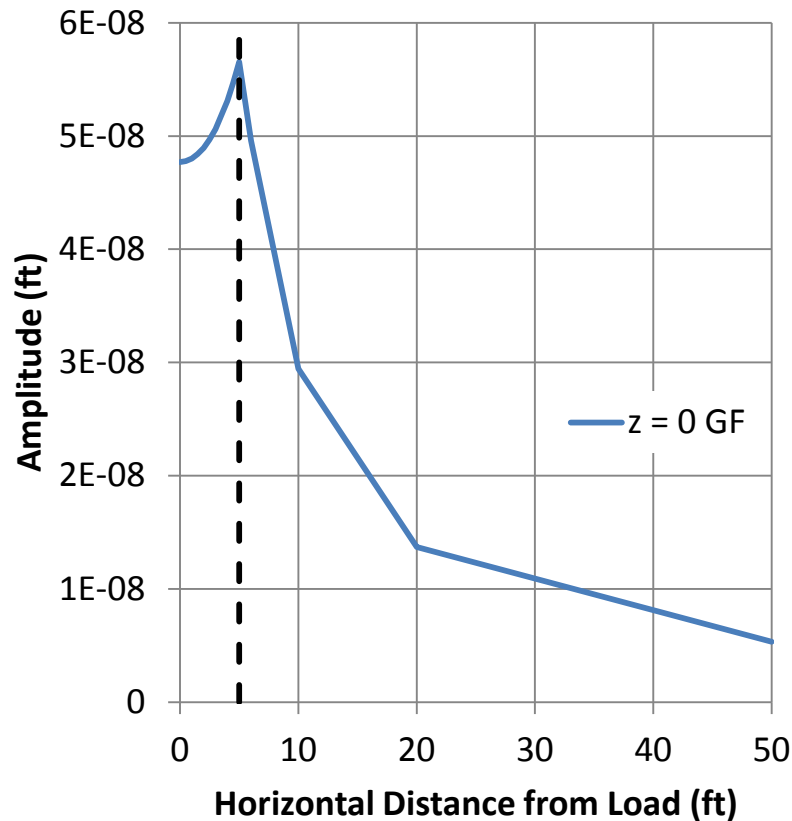
# Displacements with Transmitting Boundaries (TB)



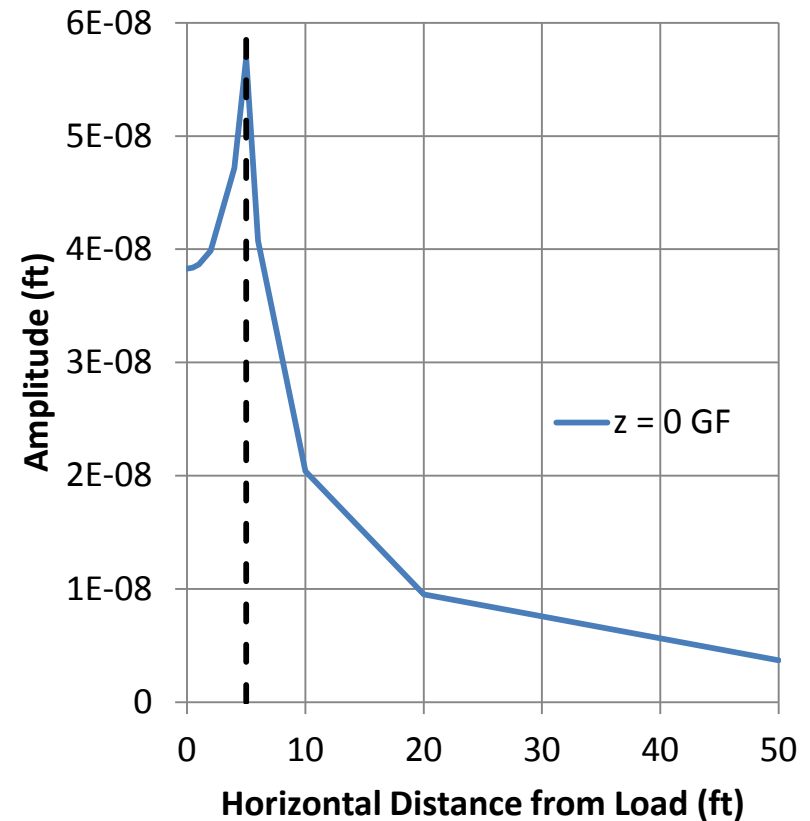
# Static Displacements at Surface – GF

Investigate displacements under the load

Frequency ~ 0. Hz – x due to x

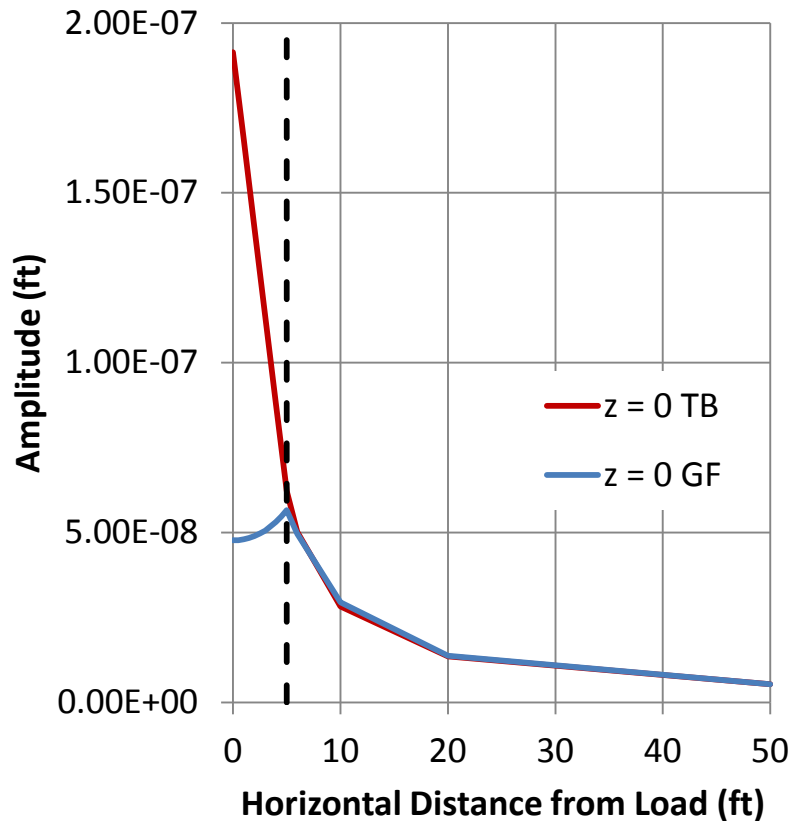


Frequency ~ 0. Hz – z due to z

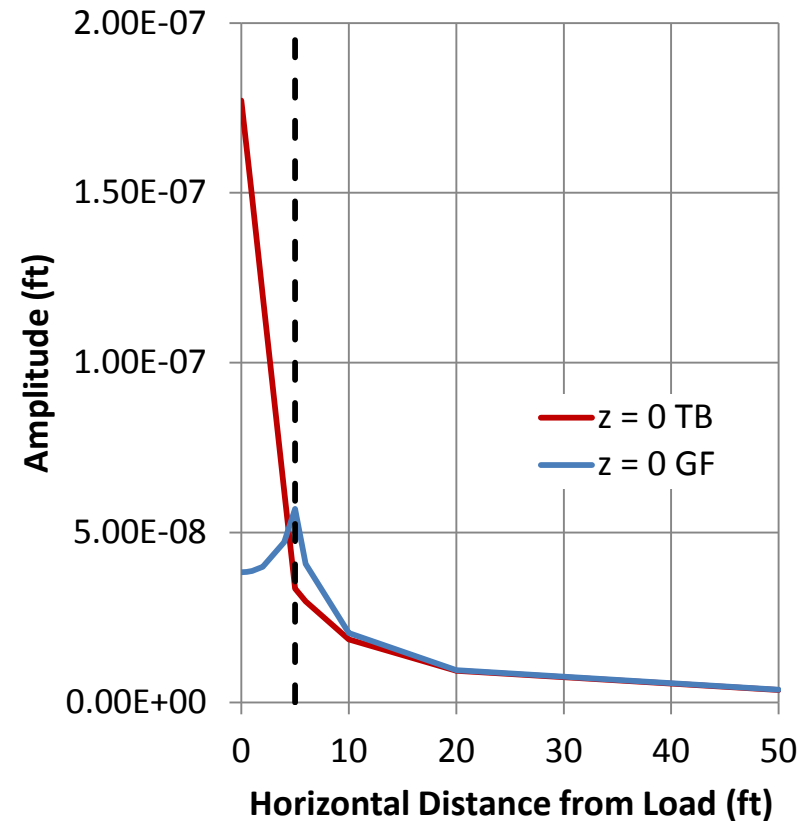


# Static Displacements at Surface – GF vs TB

Frequency ~ 0. Hz - x due to x



Frequency ~ 0. Hz - z due to z

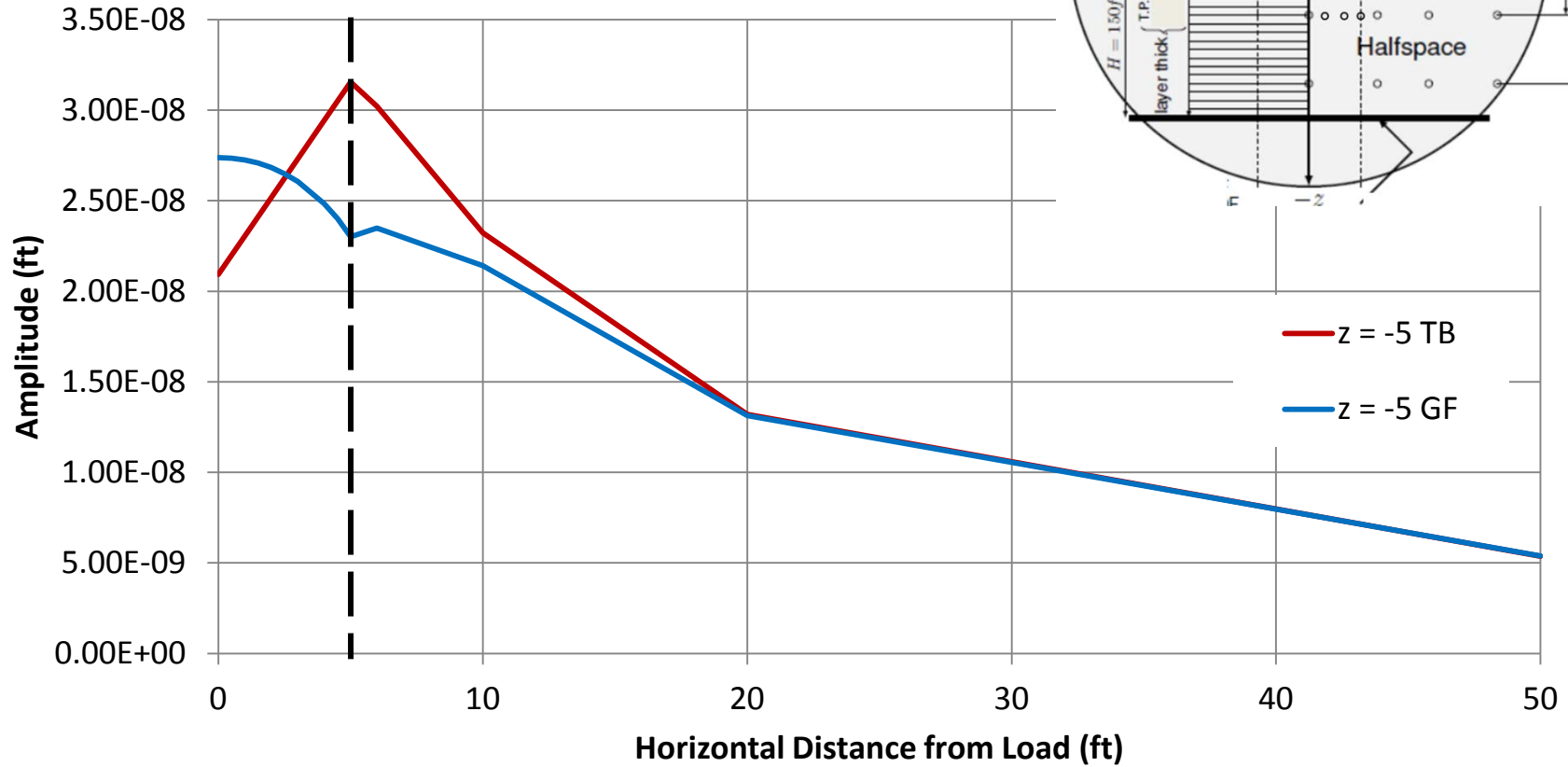


**GF: Physically consistent within the loaded area (near field) and pile/soil load transfer**  
**TB: (High amplitude) Pseudo-singularity under load: artificially high soil flexibility for piles**

# Static Displacements- x due to x- GF vs. TB

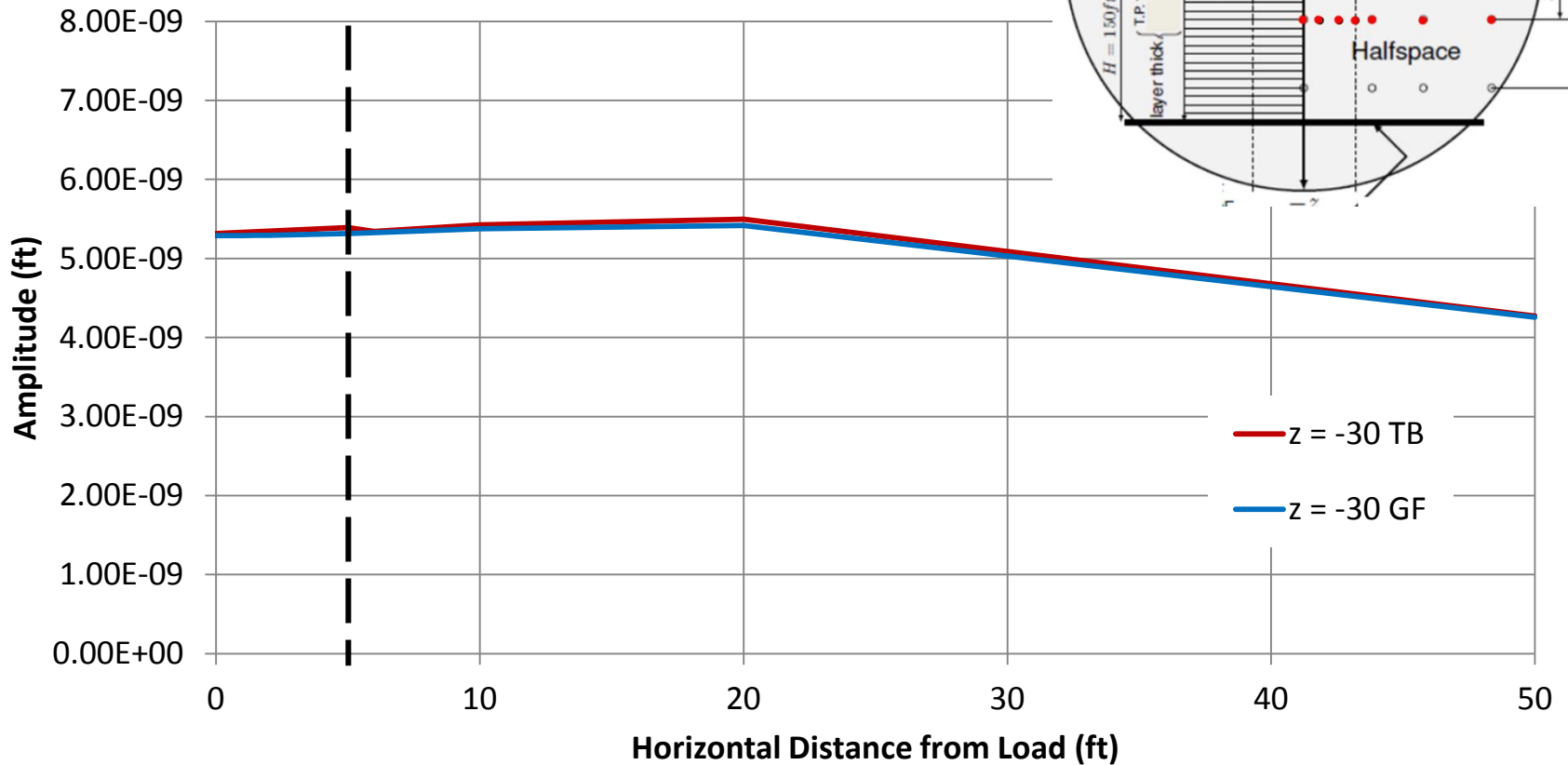
Where does TB aligns with GF for static load?

Frequency ~ 0. Hz -  $r_0=5.0$  ft



# Static Displacements- x due to x– GF vs. TB

Frequency ~ 0. Hz - r0=5.0 ft

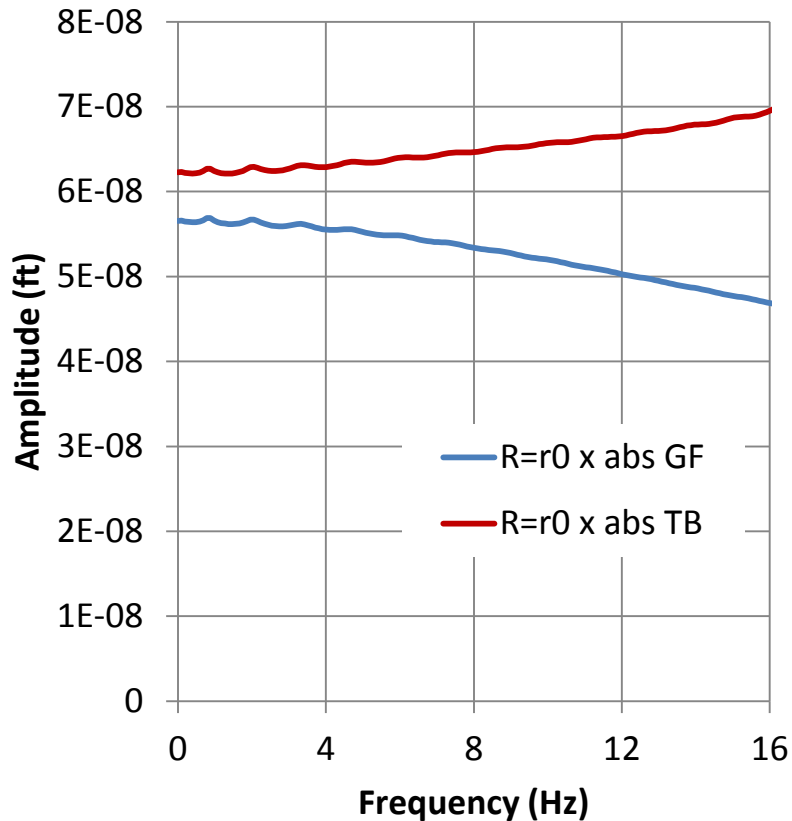


At depth from the load, static displacements TB aligns with GF

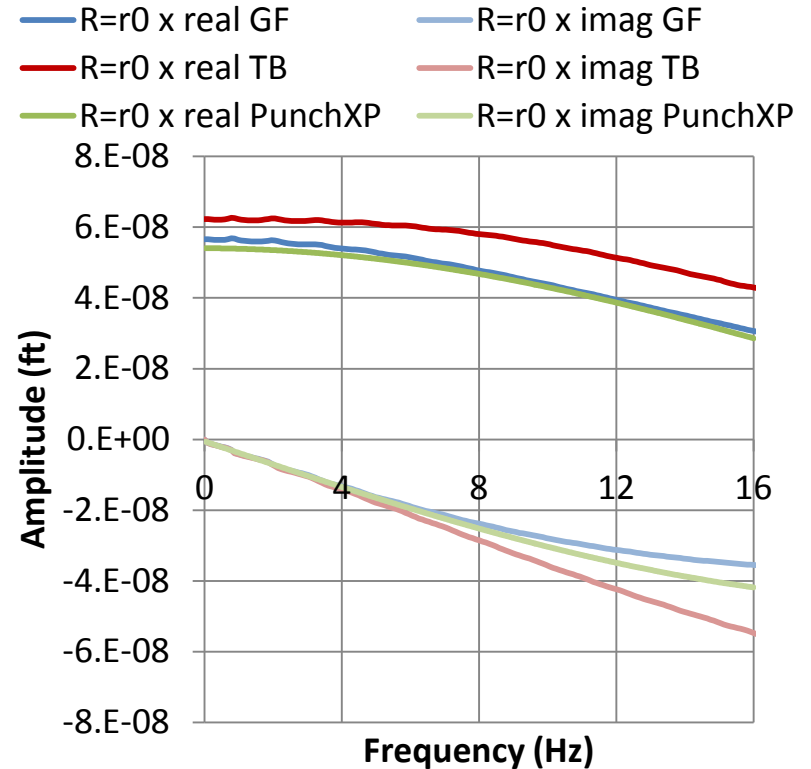
# Transfer Functions-x due to x-GF vs. TB

Where does a Ring Load behave like a Point Load  
for dynamic load?

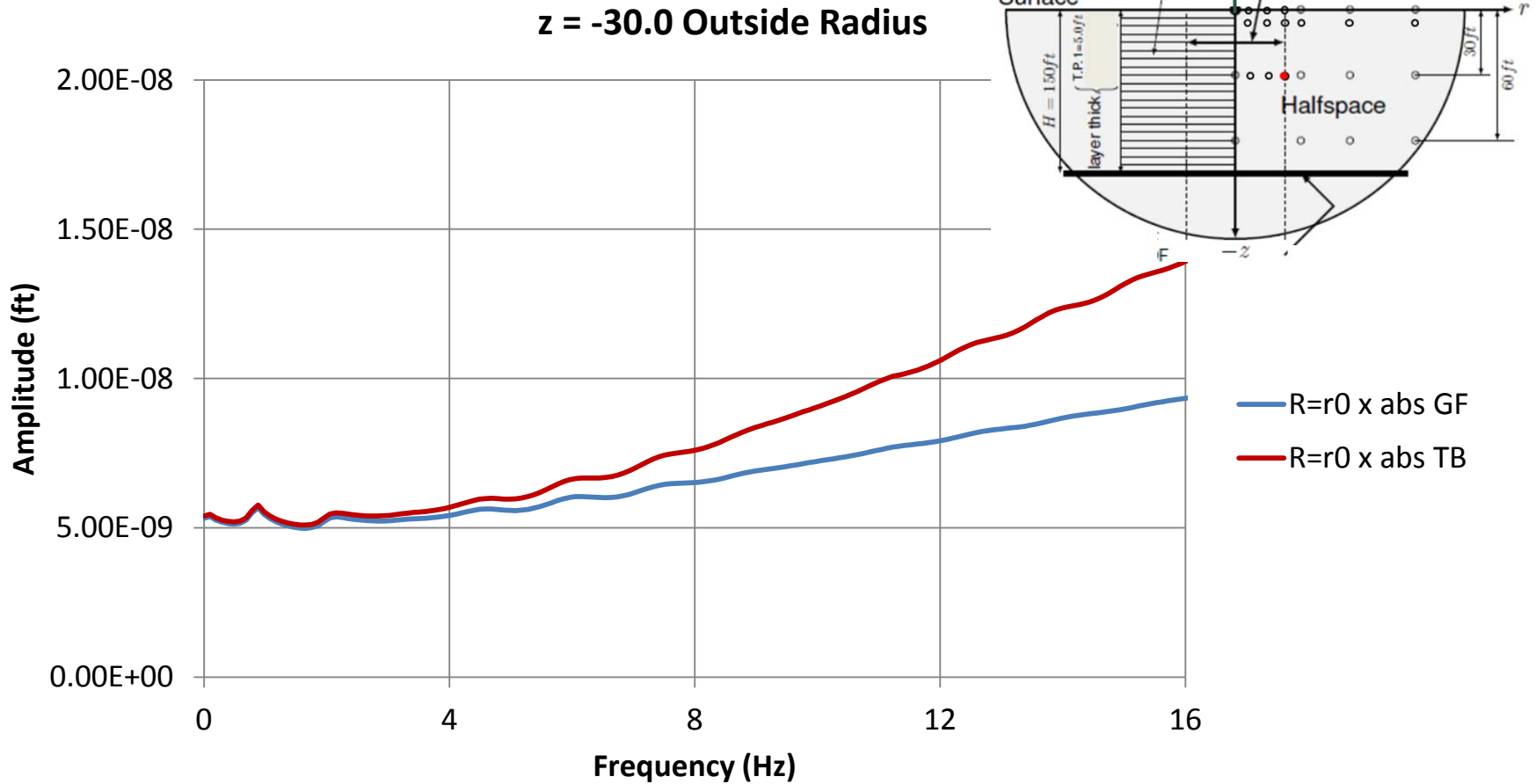
z = 0.0 Outside Radius



z=0.0 Outside Radius



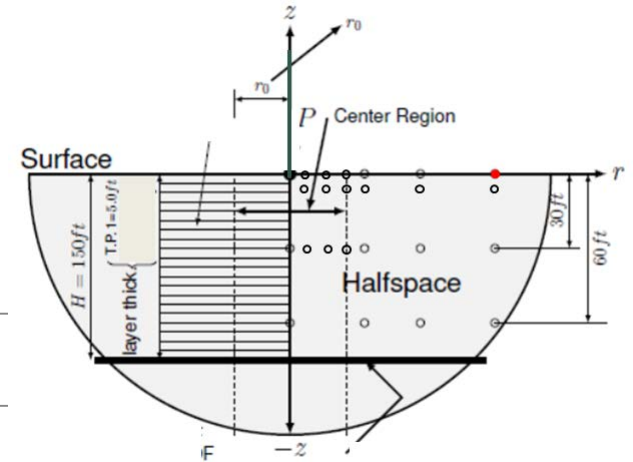
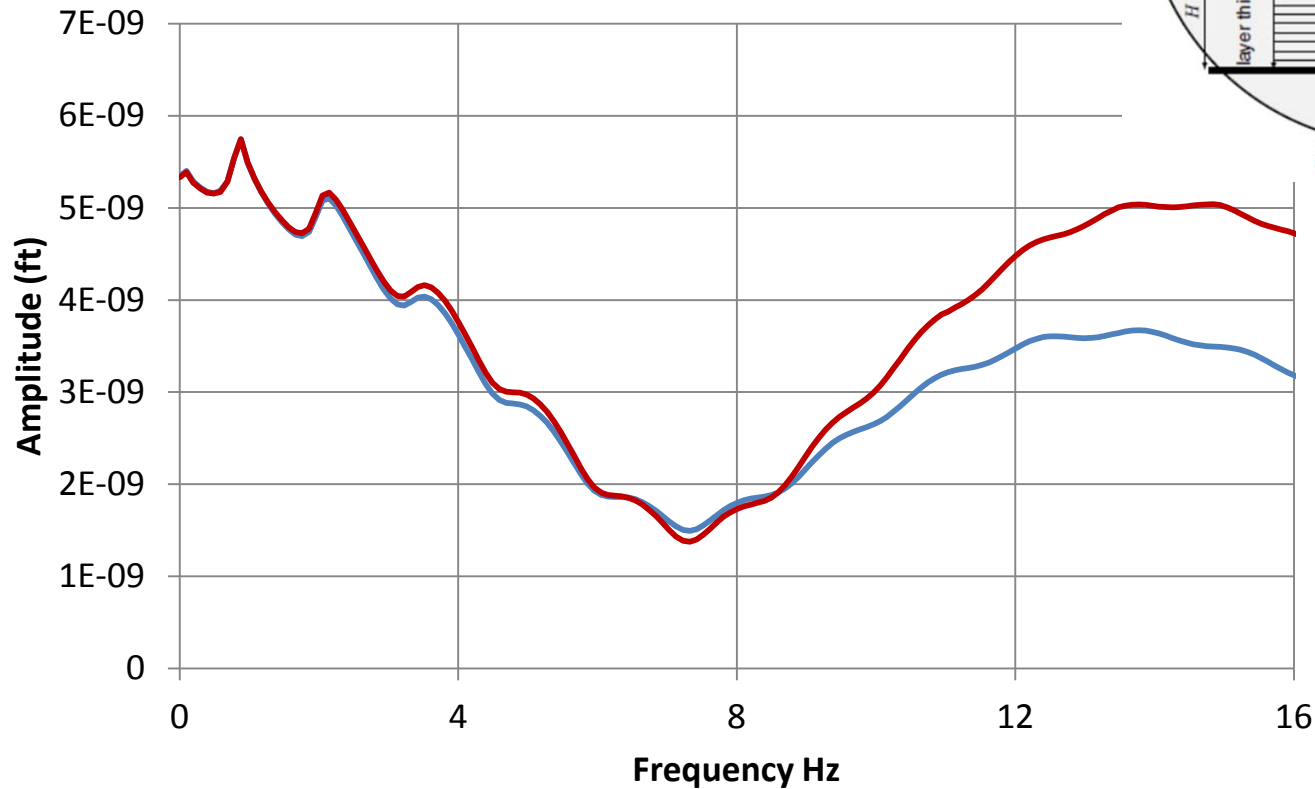
# Transfer Functions -x due to x- GF vs. TB





# Transfer Functions-x due to x-GF vs. TB

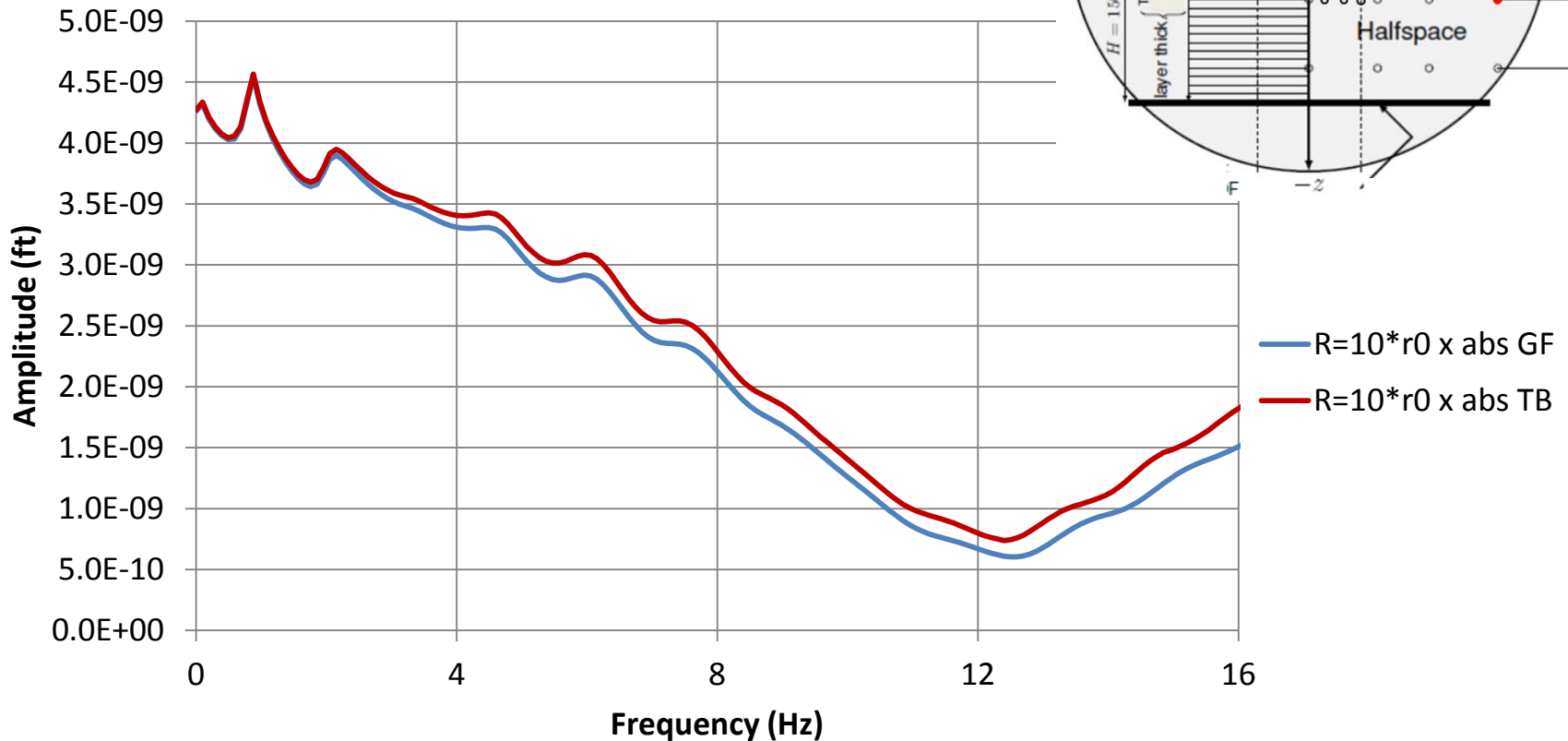
$z = 0.0$  Outside Radius



- $R=10*r_0$  x abs GF
- $R=10*r_0$  x abs TB

# Transfer Functions-x due to x-GF vs. TB

$z = -30.0$  Outside Radius

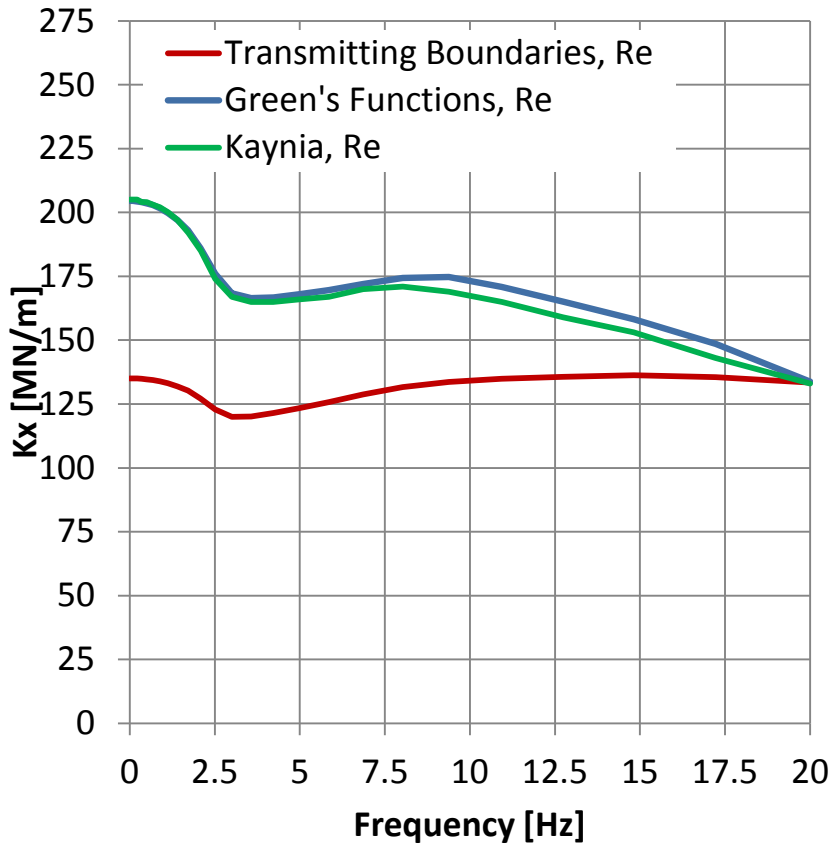


Ring Load behaves similarly to Point Load at distance and depth from the load  
 Ring/Disk Loads Green's Functions Implemented in SC-SASSI for pile simulations

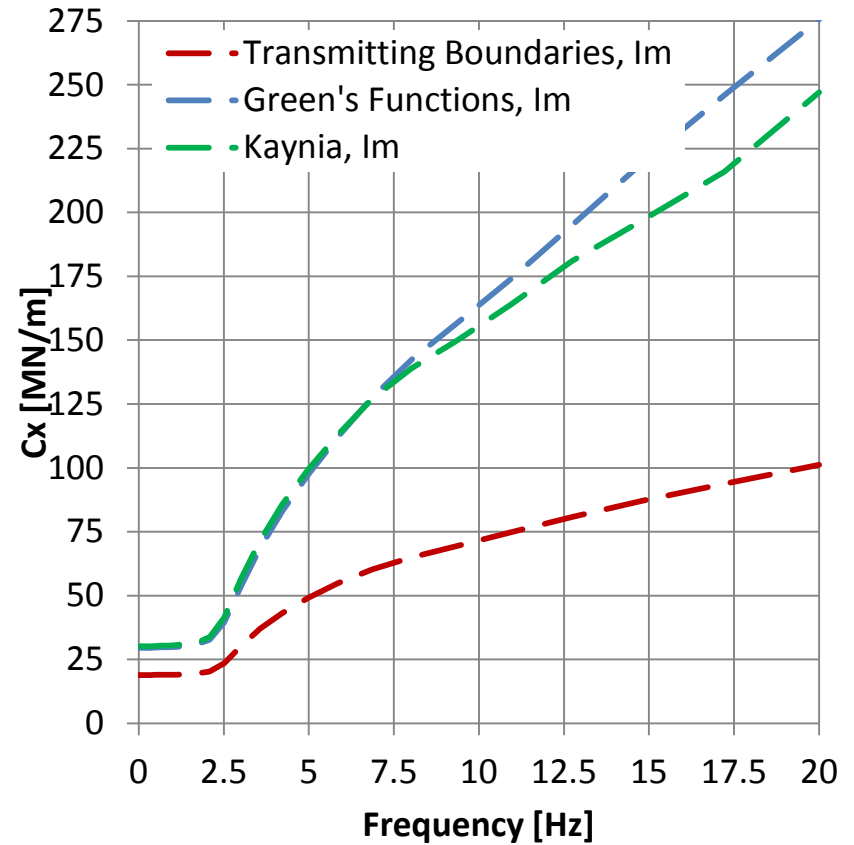
# **Dynamic Stiffness of Piles with Green's Functions using SC-SASSI**

# Dynamic Stiffness of Single Pile, Stratified Soil

## Real Component

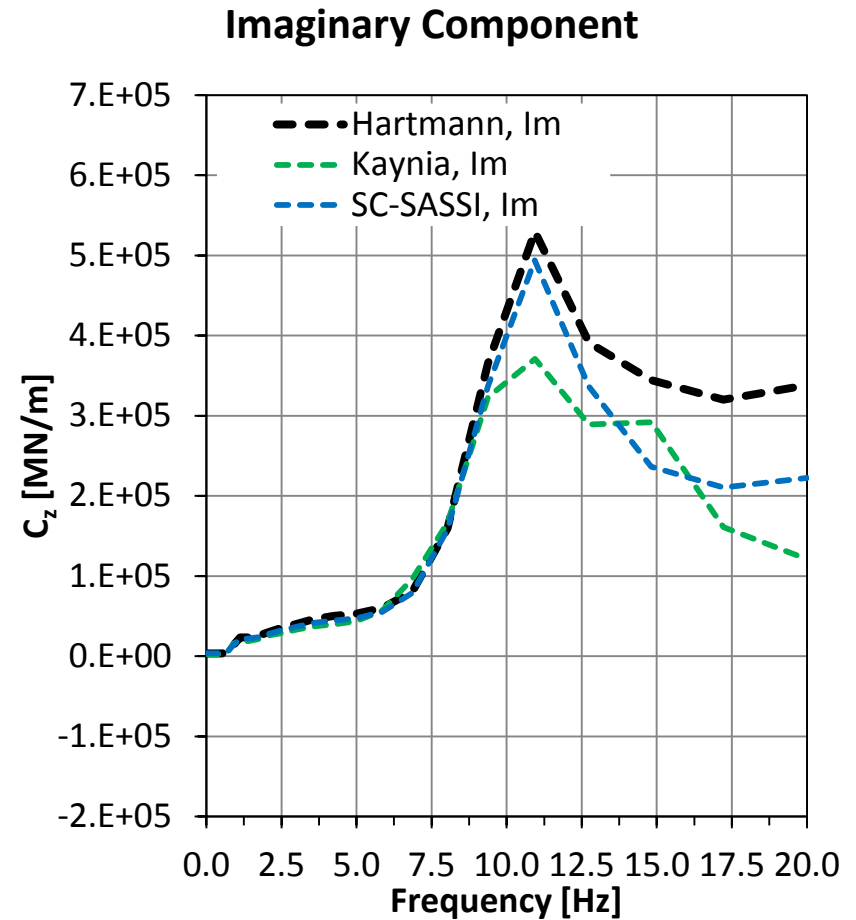
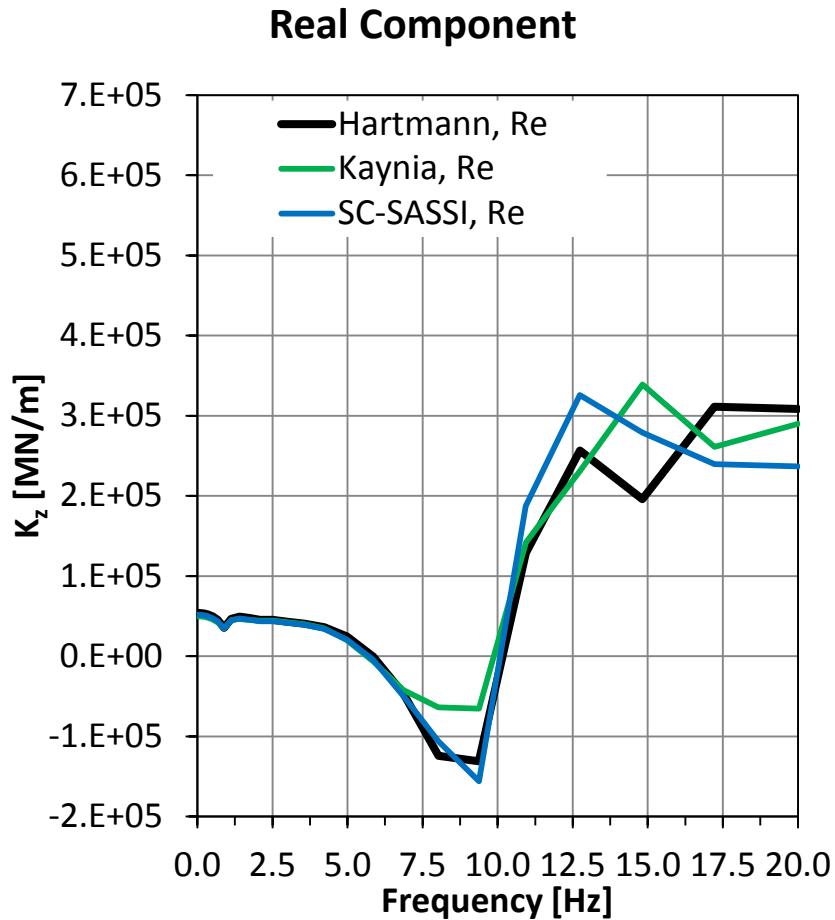


## Imaginary Component



**Green's Functions: Realistic estimate of dynamic stiffness of pile**

# Dynamic Stiffness of Group with 430 Piles

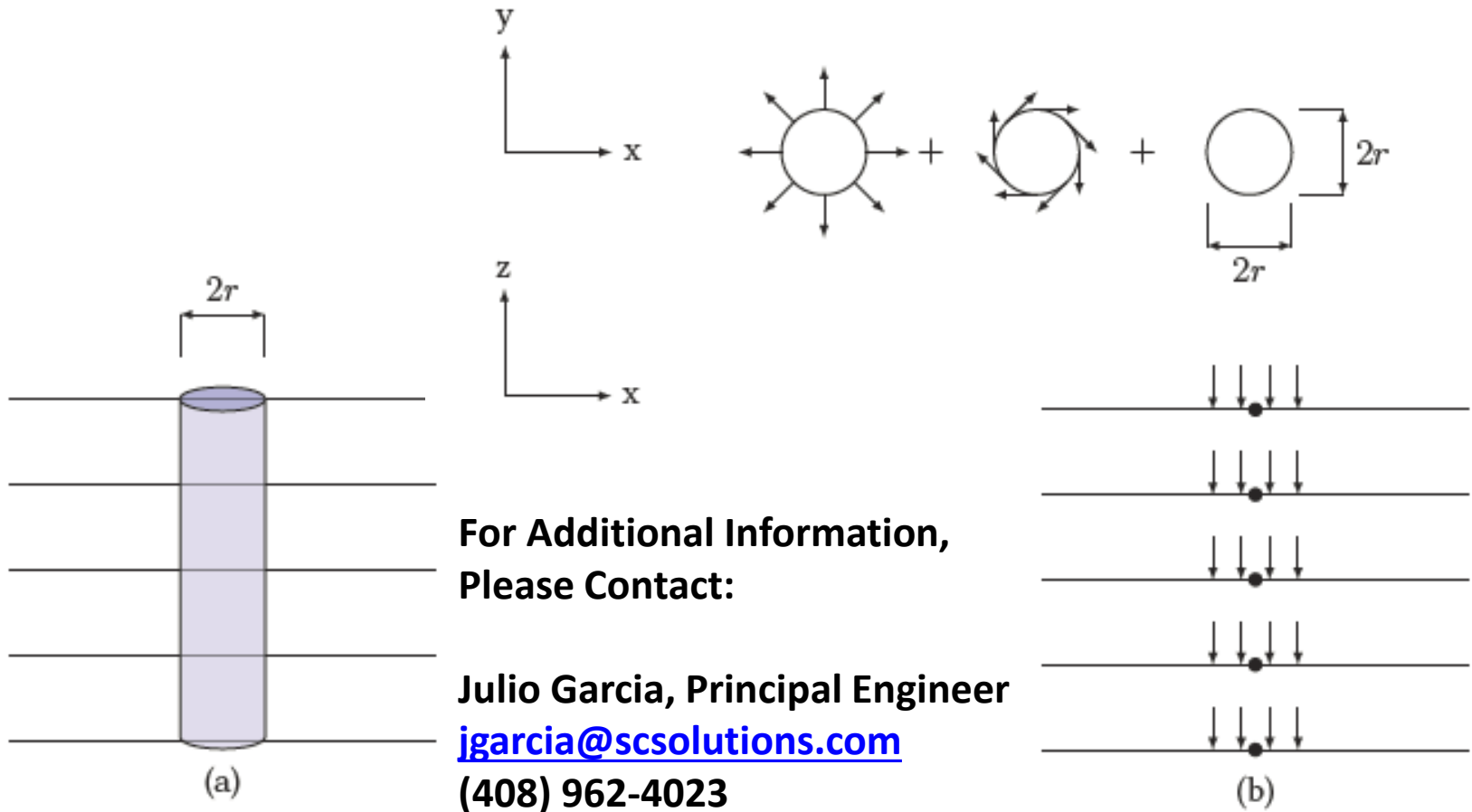


**SC-SASSI PILE simulation (GF) compares well with other independent software tools**

# Summary and Conclusions

- Transmitting Boundary approach underestimates the Dynamic Stiffness of Piles
- Transmitting Boundary shows typical singularity (high displacement amplitude) for (concentrated) Point load formulation, inconsistent with load transfer from pile to soil.
- Green's Functions for Ring and Disk (distributed) Loads show consistent behavior in near field, provides a realistic estimation of soil flexibility for piles and confirmed a suitable approach to simulate pile foundations.
- Green's Functions implementation in SC-SASSI is computationally efficient to simulate pile foundations.

# Thank you!



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